TWO MATHEMATIC MODEL FOR PREDICTION OF RESERVOIR INDUCED SEISMICITY

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With the expansion of human engineering activity both in scale and there appears an accompaning new problem --- induced seismicity in these decades especially in the last two decades. Many activities would intensify seismicity, such as impoundmen water in reservoir, large scale opencut mining and underground mining, waste liquid disposal, geothermal power generation as well as filling of high pressure water into the ground for a second time of petrolium exploitation, large scale drawing of underground water in cities and the post effect of underground nuclear detonation, ets. Since induced seismicity are accompanying engineering projects and occur near the large engineering projects triggering them, obvious social and ecnomic consequences would be incurred therefore even as weak as M = 5 magnitude, an earthquake has to be taken into account. Among various kinds of induced seismicity already known, reservoir induced seismicity (usually called reservoir earthquake) is most worth heeding. The Xinfengjiang Reservoir in China, the Kremasta Reservoir in Greese, the Kariba Reservoir in the border area between Zambia and Zinbabwe and the Koyna in India, all had triggered strong earthquakes of more than 6 magnitude one after another in 1960s, and such earthquake is most serious in Xinfengjiang and Koyna.

Exploitation of hydroelectric resources is one of the most important ways to ease the energy problem for the world and especially for China. Many seismologists have been extensively information on the cases of reservoir earthquake (according to statistics, about 100 cases throughout the world and more than 10 cases in China), identifying their features, cases and trigger mechanism to find prediction methods and engineering countermeasures.

The end result of these efforts is to find out whether earthquakes

would be induced after a reservoir is filled and what would be their intensities and location. And this is also one of the key seismological problems determining the rational operation of a reservoir and its accessory facilities.

Up to recent, owing to the restriction by the inadquate exposure of the natural phenomenon and the complicity of the problem, thus the people's poor understanding of it, extreme countermeasures have often been taken in engineering practice^[1]. In view of the low occurance probability especially for strong earthquake, some people advocate to take no consideration of the risk while others hold that the highest magnitude so far (Koyna, Ms6.5) be adopted as a general seismic protection standard for all large reservoir to be built. However, from the viewpoint to solve the contradiction between safety and economics, these two ideas both seem a little too extreme.

The scholar of different fields suggested many empirical or semi-empirical prdiction methods. [15]. In this study, The author tries to use digitally processed data from existing reservoirs (including those induced or not induced seismicity) to establish a mathematical prediction model. Here a brief description is firstly given of the statistical examination model (SEM) proposed by Packer [15] and Beacher [14]. Then the author's fuzzy comprehensive estimation model (FCEM) is presented. It goes without saying that since this mathematic prediction model is based on the analysis of existing data, it is of limitation in nature. However it is still a method which may be used inconjuction with the above methods for comprehensive judgement.

I. Statistical Examination Model for Reservoir Earthquake (SEM)

1.Used data

Since there are several hundred thausands of reservoirs in the world, it is impossible to collect all data from so numerous reservoirs. On the other hand, the seismic cases of existing reservoirs show that they (especially strong ones) occurred mostly at large reservoirs of only several hundreds in number. Also, once a large reservoir suffers an earthquake, disasterous effect would result. Therefore, data used in this analysis are limited to large reservoirs both induced (RIS) or not yet seismicity (RIS). Of course, the predictive result thus obtained are also only applicable to large reservoirs", while used on small reservoirs" it is quite possible to overestimate the inductive risks.

Seirmoinductive factors (Table 1) used in statistic analysis of large

reservoirs are considered as in close relationship with seismoinductive effects and can be found in published literature. Other possibly related factors are not listed for the time being either because they not available or because their seismoinductive effects have already been included in other factors. Once data are complete, they can be introduced into the model without difficulties.

"Large reservoir" defined in SEM and in FCEM refers to a reservoir of more than 92 meter in depth (ont the dam hight) and/or more than 10¹⁰ cubic meters in volume. The number of reservoir, used in SEM, meeting the above difinition are 29 seismoinduced and 205 no seismoinduced.

For seismoinductive factors and their classification (called factor state) see Table 1.

Based on the data of the 29 seismoinduced and 205 no seismoinduced, the frequency of the reservoirs under different states and their likelihood are listed in Tadle 2.

Table 1	Inductive	factors and their st	ates
factor		sstate	
	1	2	8
Depth(C)	d1: <15.m	d2: 92-150m	d s: <92m
Volume(V)	v ₁ : 10 ¹⁰ m ³	v ₂ : (0.12—1)10 ¹⁰	vs: 0.12·1.10 m8
Stress field(D)	sı: extensional (thrust fault circumstance)	sa: extensional (thrust fault circumstance)	ss: shear (shear fault circumstance)
Fault activity(F)	f ₁ , active	f2: inactive	
Geology condition(G)	g ₁ : sedimentary	g2: metamophic	gs: igneous

Table 2 Factor states and their likelihood rates state factor number of reservoirs 2 8 1 I(0.04) D 29 10(0.34) 18(0.62) v 29 7(0.24) 11(0.38) 11(0.38) RIS S 29 4(0:14) 18(0.26) 7(0.24) F 7 7(1.00) 0(0) G 7(0.25) 28 13(0.46) 8(0,29) 83(0.16) D 204 27(0.13) 144(0.71) v 205 52(..25) 36(0.18) 217(0.57) RIS S 203 34(0.17) 138(0.68) 81(0.15) F 6 4(0.67) 2(0.33) G 44(0.26) 165 57(0.35) 64(0.39)

2.SEM

⁽¹⁾ single factor model

It is obvious that a reservoir earthquake can not be induced only by and single one of the above factor, but a single factor is the basis for multifactor prediction model. For a known factor state, for example d_i, according to Bayes's theorem, the the conditional probability p(RIS/d_i) will be

$$q(RIS/d_i) = \frac{p(RIS) p(d_i/RIS)}{p(RIS)p(d_i/RIS + p(\overline{RIS})p_i/\overline{RIS})}$$
(1)

where p(RIS) and p(RIS) are she pre-examination probabilities of RIS and \overline{RIS} respectivery, and P(d₁/RIS) and p(d₁/RIS are the conditional pobability of RIS and RIS versus d₁ respectively.

Conditional probability (Table 3) for all single factor states can be calculated in the same way.

Table 3 conditional probability of single factor states

factor		state	
	1	2	8
D	0.26	0.11	0.03
V	0.12	0.23	0.09
S	0.10	0.12	0.18
F	0.18	0	
G	0.16	0.10	0.12

(2) Multi-factor Model

Like (1), taking all 5 factors into account, the conditional probability of earthquake occurance is

$$p(RIS/D, V, S, F, G) =$$

$$p(RIS)p(D,V,S,F,G/RIS)$$
 (2)

p(RIS)p(D,V,S,F,G/RIS) + p(RIS)p(D,V,S,F,G/RIS)the conditional probability of RIS for multi-factor is p(RIS/D,V,S,F,G)

$$= \frac{p(\overline{RIS})p(D,V,S,F,G/\overline{RIS})}{p(RIS)p(D,V,S,F,G/RIS) + p(RIS)p(D,V,S,F,G/\overline{RIS})}$$
(3)

Divide equation (2) by (3), we have

$$\frac{p(RIS/D, V, S, F, G)}{p(\overline{RIS}/D, V, S, F, G)} = \left[\frac{p(RIS)}{p(RIS)}\right] \left[\frac{p(D, V, S, F, G/RIS)}{p(D, V, S, F, G/RIS)}\right]$$

$$= \left[\frac{p(RIS)}{p(RIS)}\right] LR(D, V, S, F, G) \tag{4}$$

LR(D, V, S, F, G) in equation (4) is called likelihood ratio which can easily be obtained using figures in Table 2(see Table 4).

Table 4		likelihood ratio	
factor		state	
	1	2	3
D	2.62	0.87	0.21
· v	0.95	2.15	0.66
S	0.82	0.91	1.58
F	1.05	0	
G	1.34	0.74	0.94

I.FCEM of RIS

It should be said that the above said statistical examination model (SEM) is rigorous in the sense of statistics, but the following problems are worth approaching. Firstly, the data used above of RIS and RIS are apparently not sufficient for the examination of a nutural phenomenon jointly caused by so numerous and complicated factors. At the mean time, it can hardly be expected to supplement more data by constructing a number of large reservoirs in few years, and then it is neccessary to do more subjective judgements. Secondly, according to some studies, different factors differ greatly from each other in the relationship with RIS, this indicates that the "contributions" of different factors to seismoinduction can not be regarded as equal, and different factors as well as their states should be attached with different weights as the case may be. Thirdly, this model gives only the risk probability of RIS and does not estimate the possible maximum intensity of RIS. Obviously if estimation of RIS intensity is given, design work would be greatly facilitated. Therefore we suggest a FCEM on the basis of ad ditional data, especial data from China.

1. Fuzzy relation analysis

As pointed out above, reservoir earthquakes are caused by the combined effect of numerous factors and the seismoinductive factors are not in very close relationship with induction risk as well as possible induced intensity. For example, while high-dam large reservoirs are liable to induce earthquake, strong induced earthquakes are also seen with low-dam small reservoirs. What is the meaning of "high and large", "low and small" concerned in respect of inductive effect, reservoir depth and reservoir volume can not but be two fuzzy variables. Also, if the fault activity at and near the reservoir area is very important for judging induction effect of the fault, then what amplitude and speed of fault motion with which fault activities were to be classified are also fuzzy variables, and so on and so forth. Therefore, for the purpose of calculation, while fuzzy variables are classified, as done in SEM, it is neccessary to take

consideration of such fuzzy nature to further fuzzify them (see later). So, in view of the unfull exposure of this natural phenomenon plus the differences in contribution to inductive effect by different factors, it proves to be an effective method in practical comprehensive examination of fuzzy mathematics to give proper weights to different factors and their states according to the trend shown in existing data and the conception of the expert.

2.FCEM

The principl and methodology of reservoir earthquake prediction using FCEM had been presented elsewhere [15, 16], here given is only a chief descriotion of them.

Assumed is that the domain of intensity of reservoir induced earhquake (called intensity domain, for short)

$$V = \{ V_1, V_2, \dots, V_m \}$$
 (5)

and the domain of factor partcipating in seismoinduction (called factor domain, for short)

$$U = \{U_1, U_2, \dots, U_n\}$$
 (6)

 $U = \{U_1, U_2, \dots, U_n\}$ where m (here m = 3 is taken) and n (here n = 5) are the classes of intensity domain and the number of induction participating factors respectively.

Also assumed is that the single factor examination by ith factor to various intensity classes is

$$R_i = (r_{i1}, r_{i2}, \dots r_{im})$$
 (7)

where Rix is the membership degree of the ith factor on the kth intensity class. If expressed by matrix, the fuzxy relationship will be

$$R = \begin{pmatrix} R_{1} \\ R_{2} \\ \vdots \\ R_{n} \end{pmatrix} = \begin{pmatrix} r_{11} & r_{12} & \cdots & r_{1m} \\ r_{21} & r_{22} & \cdots & r_{2m} \\ \vdots & & & & \\ r_{n1} & r_{n2} & \cdots & r_{nm} \end{pmatrix}$$
(8)

To perform fuzzy examination of reservoir induced earthquake is in fact to investigate the fuzzy subset A in domain U and through fuzzy relation matrix R to perform image on the fuzzy subset B in intensity domain V.

The factors subset in domain U is expressed as

$$A = \frac{a_1}{U_1} + \frac{a_2}{U_2} + \dots + \frac{a_n}{U_n}$$
 (9)

where a_1 , a_2 , ..., a_n are the membership degree of $U_1 \cdots U_n$ that is the peoples weighting of the factors effects on seismoinduction and its possible intensity, or the contribution by them to the seismoinduction (weight distribution).

The fuzzy subset of intensity domain is assumed as

$$B = \frac{b_1}{V_1} + \frac{b_2}{V_2} + \dots + \frac{b_m}{V_m}$$
 (10)

where $b_1 \cdots b_m$ are the membership degree of various intensity classes on the examined intensity, and are the answeer we require. The plus and division sign in (9) and (10) are Zadeh symbols.

Now the first stage of prediction model can be expressed simply as

$$B = A \circ R \tag{16}$$

οг

$$(b_{1}, b_{2}, \dots, b_{m}) = (a_{1}, a_{2}, \dots, a_{n}) \circ \begin{pmatrix} r_{11} & r_{12} & r_{1m} \\ r_{21} & r_{22} & r_{2m} \\ \vdots \\ r_{n1} & r_{n2} & r_{nm} \end{pmatrix}$$

$$(12)$$

where "o" is the complex operation sign. In consideration of the nature of varion seismoinductive factors, here a pair of operators (•, ⊕) is used and "•" is the usual multiplication sign, "⊕" is bounded summation namely when weight vectors and the elements in relation matrix are normalized, the above operators will into a pair of operators (•, +) used in conventional summing and products.

$$\alpha \oplus \beta = \min (\alpha + \beta, 1)$$

Since the factors are classified into several factor states, it is very difficult to distribute weights to all factors at the same time. So Eq (11) and (12) are revolved into the second stage examination model

$$B = A \circ R = A \begin{pmatrix}
A_1 & \circ R_1 \\
A_2 & \circ R_2 \\
& & \dots \\
A_n & \circ R_n
\end{pmatrix}$$
(13)

where A₁—A₂ and the weight factors of various factor states 3. Factors and their states

To make comparision with SEM, factor states are changed a little, i. e., a 4th state is added and g₄ is carbonatite in kind (see Table 1).

4. Difference examination of "pair of factor states" for strong induced earthquake of equal and more than $W_{\bullet} \ge 5.0 \, (M_{\bullet\bullet\bullet\bullet\bullet})$ and weak induced earthquake less than $W_{\bullet} < 5.0 \, (M_{\bullet\bullet\bullet\bullet\bullet})$.

Apparently, to predict actual intensity is difficult due to limited data. In viewpoint of engineeing, to divide induced earthquake into two or-

der with M. 5.0 as dividing threshold is a feasible approach. To do so, it is neccessary to perform difference examination of various factor of the known earthquake of $M. \ge 5$ and $M. \le 5$. In other words, examination of order is possible only if the difference is great enough so that the induced intensites can be divided into two orders. Here we use X^2 examination. Examination of M_{macro} and M_{macro} can be made separately only when the value of actual examined X^2 for a factor state pair is greater than threshold value for 90-95% of confidence degree. Here X^2 is calculated by the formula

$$X^{2} = \sum_{i} \sum_{j} \frac{\sum_{k} \frac{(n_{ij} - n_{k} p_{i} p_{j})^{2}}{n_{k} p_{i} p_{j}}}{n_{k} p_{i} p_{j}}$$

$$p_{i} = \sum_{j} \sum_{k} \frac{n_{ijk}}{n}$$

$$p_{j} = \sum_{i} \sum_{k} \frac{n_{ijk}}{n}$$
(14)

where i means the column in the determinant for factor states, j means the row, k_1 and k_2 are the data group of M_{macro} and M_{micro} , n_{ij} is the number of reservoir in column i and row j, n^k is the total number of reservoir of M_{macro} or M_{micro} or M_{micro} i.e., $n = n_{k-1} + n_{k-2}$.

The results of difference examination are as follows (Table 5)

Pair of factor	X2	degree of	threshol	d value of
states	^-	freedom	$\alpha = 0.1$	$\alpha = 0.05$
DV	21.0	8	13.4	15.5
D-S	10.5	. 8	13.4	15.5
D—G	17.2	12	18.5	21.0
v-x	54.3	8	13.4	15.5
V—G	50.3	12	18.5	21.0
S-G	22.5	12	13.5	21.0

Table 5

Erom the result in Table 5, it can be seen that the actual values of X^2 of almost all factor state pairs exceed the threshold value of corresponding degree of free-dom except that the signification of difference of C—S and D—G are a little lower than threshold value of 90% of confidence degree. Thus it may be concluded that strong earthquake (M. \geqslant 5) and weak earthquake may be examined separayely.

5. Membership degree of single factor state (relation matrix R)

Basing on the data in Attached Table 1 (M, > 5 - Mmacra) and Attach-

ed Table 2 (M. < 5 - Mmlere) of RIS and the data in Attached Table 3 of RIS (Attached tables omitted), relation matrixes shown in Table 6 are given by statistics, the figures in parentheses are the number of corresponding reservoirs.

Tabie 6	Membership	degree	of	single	factor	states
	шешесте	3	- •	· · · · · · · · · · · · · · · · · · ·		

factor	state	Mmacro	Mmicro	М。
<u> </u>	dı	0.200(2)	0.388(12)	0.129(26)
$R_{\mathbf{D}}$	da.	0.600(6)	0.581(18)	0.693(140)
	d s	0.200(2)	0.032(1)	0.328(36)
	ν,	0.400(4)	0.233(7)	0.238(48)
R▼	V2.	0.600(6)	0.267(8)	0.188(38)
	va	0(0)	0.500(15)	0.574(116)
	s ₁	0.200(2)	0.172(5)	0.212(42)
R s	S ₂	0.400(4)	0.655(19)	0.641(127)
	S ₂	0.400(4)	0.172(5)	0.146(29)
R _F	fa.	1.000(10)	1,000(8)	0.670(4)
	fa	0(0)	0 (0)	0.330(2)
	g ₁	0.400(4)	0.074(2)	0.218(37)
Ro	ga	0.200(2)	0.333(9)	0.355(60)
	Sg	0.300(3)	0.296(8)	0.278(47)
	g4	0.100(8)	. 0.296(7)	0.148(25)

It should be pointed out that there are active faults at and nearthe areas of the 10 M_{macre} reservoirs according to data concerned and in-field investigations [13], while for M_{macre} reservoirs, only a few of them were investigated in respect of fault activity (e.g. Aksombo of Ghana Clark Hill of USA, Keben of Turkey, Nurek and Toktokyer of USSR, Sefid of Iran Danjiangkou and Foziling of China, etc.), in and near reservoir area So Rf of M_{macre} are also taken as 1.0 (f₁) and $O(f_2)$.

As said above, for reservoir depth and volume, being also fuzzy continuous variables, it is not reasonable enough to perform definite subjective clarification, for example, why 151 meter and 149 meter of depth are classified as d_1 and d_2 respectively and not in other way? Therefore, in consideration that maximum magnitude did not always occurred with highest water level and corresponding valume, a fuzzy classification membership function μ_1 is difined in the calculation of depth and volume membership degree,

$$\mu_{i} = \begin{cases} 1 & n = i \\ 0.7 & n = i - 1, & i + 1 \\ 0.3 & n = i - 2, & i + 2 \end{cases}$$
 (15)

Also, stress state, fault activity and medium condition are of fuzzy nature when they are determined from data concerned, for example, stress state are not so clear as those listed in Table 1; strike-slip with dipslip component is classified as strike-slip circumstance, it is difficult to ascertain what medium condition is prevailing for the predominant structure of a reservoir, and so on and so forth. Therefore a fuzzily classified membership function μ_i is also defined for these factors,

$$\mu_{i} = \begin{cases} 1 & n = i \\ 0.5n \neq i \end{cases} \tag{16}$$

In this way, after calculation, data in Table 6 are converted into those in Table 8.

Ta	ble	7
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actor	state	Mmacro	Mmicro	М •
	d ₁	0.304(5.8)	0.360(24.9)	0.293(134.8)
R_D	d2	0.392(8.8)	0.392(27.1)	0.399(183.4)
	d s	0.304(6.8)	0.248(17.2)	0.308(141.8)
	v1	0.366(8.2)	0.271(17.1)	0.261(109.4)
Rv	va.	0.393(8.8)	0.370(23.4)	0.365(152.8)
	v s	0.241(5.4)	0.359(22.7)	0.374(157.0)
	s ₁	0.300(8)	0.293(17)	0.303(120)
Rs	. Sg	0.350(7)	0.414(24)	0.410(162.5)
	S8	0.350(7)	0.293(17)	0.287(113.5)
RF	f ₁	0.667(10)	0.667(18)	0.556(5)
	fa	0.333(5)	0.333(4)	0.444(4)
	g ₁	0.280(7)	0.215(14.5)	0.244(103)
Rc	g ₂	0.240(8)	0.267(18.0)	0.271(114.5)
	gs	0.260(6.5)	0.259(17.5)	0.256(108)
	g₄	0.220(5.5)	0.259(17.5)	0.229(977)

6. weight vector of factor and weight vector of state

In the light of the tendences of experts abroad, reported in publicized literature and the recognition of the author, here the weight vector of factor, A, is taken as

 $A = \{0.35(D), 0.25(V), 0.20(S), 0.10(F), 0.10(G)\}$ (17)

Making reference to the published or unpublished data, weight vector of factor states is taken as

$$\begin{array}{c} d_1 \quad d_2 \quad d_3 \\ 0.20 \quad 0.60 \quad 0.20 \quad M_{\text{macro}} \\ A_D = \begin{pmatrix} 0.45 \quad 0.52 \quad 0.03 \end{pmatrix} M_{\text{micro}} \\ 0.12 \quad 0.70 \quad 0.18 \quad M_{\text{o}} \\ 0.12 \quad 0.70 \quad 0.18 \quad M_{\text{o}} \\ V_1 \quad V_2 \quad V_3 \\ A_{\text{o}} = \begin{pmatrix} 0.30 \quad 0.60 \quad 0.10 \\ 0.24 \quad 0.31 \quad 0.45 \end{pmatrix} M_{\text{micro}} \\ 0.23 \quad 0.19 \quad 0.58 \quad M_{\text{o}} \\ S_1 \quad S_2 \quad S_3 \\ 0.20 \quad 0.40 \quad 0.40 \quad M_{\text{macro}} \\ A_S = \begin{pmatrix} 0.21 \quad 0.58 \quad 0.21 \end{pmatrix} M_{\text{micro}} \\ 0.21 \quad 0.63 \quad 0.16 \quad M_{\text{o}} \\ f_1 \quad f_2 \\ 1.00 \quad 0 \quad M_{\text{macro}} \\ A_{\text{f}} = \begin{pmatrix} 0 \quad 1.00 \end{pmatrix} M_{\text{micro}} \\ 0.67 \quad 0.33 \quad M_{\text{o}} \\ 0.30 \quad 0.30 \quad 0.30 \quad 0.10 \quad M_{\text{macro}} \\ A_G = \begin{pmatrix} 0.09 \quad 0.35 \quad 0.30 \quad 0.26 \end{pmatrix} M_{\text{micro}} \\ 0.22 \quad 0.36 \quad 0.27 \quad 0.15 \quad M_{\text{o}} \\ \end{array}$$

(18)

I. Predictive tables of two models (SEM and FCEM)

1. Predictive table for SEM

Basing on the figures in Table 4 and using Fq. (4), the seismoinductive probability of combination of 162 ($3 \times 3 \times 3 \times 2 \times 3$) factor states, assuming varoius seismoinductive factors are probabilistic independent (last row), are calculated.

2.Predictive table fro FCEM

Basing on the relation matriex in Table 7 and the factor weight vector (Eq. 17) and factor weight matrix (Eq. 18), the predictive results of the seismoinductive possibility and possible inducing intensity for combination of 216 ($3 \times 3 \times 3 \times 2 \times 4$) factor states are calculated (last two row in Table 8. Also, the normalized membership degree of b_2 and b_3 of various classes on the fuzzy comprehensive evaluation are given in Table 8.So, not only predict the intensity classes, but also may known the risk of various intensity class based on their membership degree.

Having the two predictive tables, the predictive result may be examined at once, once the states of five seismoinductive factors of a large reservoir to be predicted are determined.

In order to examinate the success of two models, according to

11 12 12 13 13 15 15 15 15 15 15 15 15 15 15 15 15 15		b2 0.465 0.471 0.479 0.386 0.397	d ₁ v ₁ b ₃ 0.119 0.119 0.113	FCEM				d1				-	dt vs	Magar	M H Z
		b2 0.465 0.471 0.470 0.386 0.397 0.396	bs 0.119 0.119 0.113	FCEM	1							-		1,000	CEM
		0.465 0.471 0.470 0.386 0.397	0.119 0.119 0.113		SEM				FCEM	SEM			<u>.</u>	MHOH	יייים כי
· J · J		0.465 0.471 0.470 0.479 0.386 0.397	0.119 0.119 C.113	prediction	tion	1	8 O	 6	prediction	tion	10	5 3	n	prediction	ion
, d		0.471 0.470 0.479 0.386 0.397	0.119	Mmicro	0.358	0.436	0.449	0.083	Mmacro	0.558	0.343	0.408	0.190	Mmicro	0.280
		0.470	C.113	Mmicro	0.235	0,461	0.454	0.085	Mmicro	0.411	0.338	0.473	0.189	Mmicro	0.176
, d		0.386		Mmicro	0.282	0.468	0.453	0.079	Mmacro	0.470	0.346	0.472	0,182	Mmicro	0.214
		0.396 0.397 0.396	0.108	Mmicro		0.465	0.401	0.074	Мтасго		0.340	0.481	0.179	Mmicro	
, 4		0.397	0.307	Mmicro	0.271	0.404	0.375	0.221	Мтасто	0.457	0.199	0.394	0.407	Мо	0.205
		0.396	0.301	Mmicro	0.170	968.0	0.385	0.219	Mmacro	0,317	0.197	0.405	0.398	Mmicro	0.125
5 60 8	-	_	0.290	Mmicro	0.207	0.406	0.384	0.210	Mmacro	0.371	0.210	0.403	0.387	Mmicro	0.153
		0.409	0.287	Mmicro		0.400	0.394	0.206	Mmacro		0.198	0.416	0.386	Mmicro	
-	0.375	0.472	0.153	Mmicro	0.382	0.423	0.457	0.120	Mmicro	0.584	0,311	0.475	0.213	Mmicro	0.301
	0.370	0.476	0.154	Mmicro	0.255	0.418	0.461	0.121	Mmicro	0.436	0.308	0.480	0.212	Mmicro	0.192
fı	0.377	0.475	0.148	Мтісто	0.303	0.424	0.460	0,116	Mmicro	0.496	0.315	0.479	0.206	Mmicro	0.232
) 60 -	0.372	0.483	0.144	Mmicro		0.421	0.467	0,112	Mmicro		0.310	0.486	0.204	Mmicro	
22	0.272	0,414	0.313	Mmicro	0.292	0.354	0.401	0.244	Mmicro	0.483	0,186	0.421	0.394	Mmicro	0.223
	0.269	0.422	0,309	Mmicro	0.186	0.349	0.409	0.242.	Mmicro	0.340	0.185	0.429	0.386	Mmicro	0.136
fz	0.279	0.421	0.300	Mmicro	0.225	0.358	0.408	0.235	Mmicro	968.0	0,195	0.428	0.377	Mmicro	0.167
* 80	0.271	0.432	0.298	Mmicro		0.352	0.417	0.231	Mmicro		0.186	0.438	0.376	Mmicro	
, K	0.441	0,466	0.094	Mmicro	0.518	0.487	0.450	0.063	Mmacro	0.709	0.369	0.470	0.161	Mmicro	0.428
	0.434	0.471		Мтісто	0.373	0.480	0.455	0.065	Мтасго	0,573	0.364	0.474	0.162	Mmicro	0.292
f ₁	0.441	0.470		Mmicro	0.430	0.486	0.454	090.0	Мтасго	0.631	0.371	0.473	0.155	Mmicro	0.344
83	0.437	0.478	0.084	Mmicro		0.484	0.462	0.055	Мтасто		0.367	0.482	0.151	Mmicro	
SS	0.357	0,395	0.248	Mmicro	0.418	0.437	0.383	0.180	Mmacro	0.619	0.252	0.404	0.343	Mmicro	0.332
) 84 	0.350	0.405	0.245	Mmicro	0.284	0.429	0.392	0.179	Mmacro	0.473	0.249	0.413	0.337	Mmicro	0.216
f. g	0,361	0.404	0.235	Mmicro	0.335	0.438	0.391	0.171	Mmacro	0.532	0.260	0.412	0.327	Mmicro	0.259
- 48	0.353	0.416	0,231	Mmicro		0.433	0.401	0.160	Мтасго		0.251	0.424	0.325	Mmicro	

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	SEM	tion	0.114	0.066	0.083		0.079	0.045	0.057		0.125	0.073	160.0		0.087	0.050	0.063		0.199	0.120	0.148		0,142	0.083	0.104	
	FCEM	prediction	Mmicro	Mmicro	Mmicro	Mmicro	Мо	Мо	Mo	Мо	Mmicro	Mmicro	Mmicro	Mmicro	Mo	Mo	Мо	Мо	Mmicro	Mmicro	Mmicro	Mmicro	Mo	Мо	Μo	Mo
d b	ءً.	5	0.321	0.318	0.311	0.310	0.567	0.653	0.544	0.546	0,324	0.321	0.316	0.314	0.523	0.513	909.0	0.507	0.288	0.385	0.280	0.278	0.499	0.489	0.480	0.481
		3	0.352	0.359	0.358	0.365	0.235	0.249	0.249	0.256	0.375	0.381	0.380	0.386	0.290	0.300	0.299	0.306	0.361	0.367	0.366	0.373	0.257	0.270	0.269	0.276
	-4	,	0.327	0 323	0.330	0.325	0.198	0.197	0.208	0.198	0.301	0.298	0.304	0.300	0.187	0.187	0,195	0.187	0.351	0.348	0.354	0.349	0.244	0.242	0.251	0.243
	SEM	tion	0.295	0.188	0/227		0.219	0,133	0.164		0.317	0.204	0.246		0.237	0.146	0.179		0.447	0.308	0.362		0.350	0.229	0.274	
	FCEM	prediction	Mmacro	Mmacro	Мтасго	Mmacro	Mo	Mo	Mmacro	Mo	Mmacro	Mmacro	Mmacro	Мтасго	Mo	Mo	Мо	Mo	Mmacro	Mmacro	Mmacro	Mmacro	Mmacro	Mmacro	Мтасго	Мшасго
dg VB		•	0.215	0.214	0.208	0.206	0.390	0.083	0.375	0.374	0.231	0.230	0.225	0.223	0.380	0.374	0.368	0.367	0.130	0.189	0.184	0.181	0.340	0.336	0.328	0.326
	•	•	0.343	0.350	0.350	0.356	0.235	0.248	0.248	0.254	0.365	0.371	0.370	0.376	0.284	0.294	0.293	0.299	0.350	0.357	0.356	0.362	0.254	0.265	0.265	0.271
			0.441	0.436	0.442	0.438	0.375	0.369	0.377	0.372	0.404	0.399	0.405	0.402	0.336	0.332	0.339	0.334	0.460	0.454	0.460	0.457	0.406	0.399	0.402	0.407
	SEM	ion	0.156	0.093	0.115		0.110	0.064	0.080		0,171	0,102	0.126		0.120	0.071	0.088		0.263	0.165	0.200		0.192	0.116	0.143	
	FCEM	prediction	Mmicro	Mmacro	Mmacro	Мтасго	Mo	Mo	Mo	Мо	Mmicro	Mmicro	Mmicro	Mmicro	Mo	Mo	Мо	Мо	Mmacro	Mmacro	Mmacro	Мтасго	Мо	Mo	Mo	Мо
d2 v1	ءً.	•	0.262	0 260	0.254	0.251	0.491	0 480	0.470	0.471	0.273	0.271	0.265	0.263	0.459	0.450	0.430	0.443	0.231	0.230	0.224	0.221	0.424	0.416	0.407	0.407
		;	0.346	0,353	0,353	0.360	0.220	0.236	0.235	0.243	0.369	0.375	0.375	0.381	0.279	0.290	0.289	0.296	0.354	0.361	0 360	0.366	0.243	0.257	0.256	0.263
		10	0.392	0.386	0.393	0.389	0.289	0.284	0.295	0.287	0.358	0.354	0.360	0.356	0.262	0.260	0.268	0.261	0.415	0.410	0.416	0.413	0.322	0.327	0.337	0.330
			18	₽0 e 6	. 5	8 4	13	88	8.8	. 43	18	88	83	84	8	8 0	88	84	81	88	80	8.4	83	88	\$	8
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续 表

Table 8

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		1	-4	4	FCEM	SEM	غ.	2.		FCEM	SEM	ė	, .	ءً.	FCEM	SEM
		5	N O	5 ·	prediction	tion	•	a 0	•	prediction	tion	.	•	3	prediction	tion
	19	0.398	0.343	0.272	Мшасго	0.043	0.463	0.329	0.208	Mmacro	0.092	0.310	0.339	0.351	Mo	0.030
-	88	0.391	0.340	0.269	Mmacro	0.024	0.455	0.338	0.207	Мтасго	0.053	0.305	C.349	0.346	Mmicro	0.017
-	88	0.401	0.340	0.269	Мпасго	0.030	0.463	0.337	0.200	Mmacro	990.0	0.315	0.348	0.338	Mmicro	0.022
	8	0.395	0.339	0.257	Мтасго		0.459	0.345	0.196	Мтасго		0.305	0.348	0.327	Mmicro	
- Is	50	0.229	0.103	0.670	Mo	0.029	0.375	0.152	0.473	Мо	0.063	0.084	0.136	0.780	Mo	0.021
	64 50	0.225	0.134	0.641	Mo	0.016	0.366	0.175	0.459	Мо	0.036	0.088	0.164	0.748	Мо	0.013
5	50 50	0.243	0.133	0 624	Мо	0.021	0.379	0.175	0.446	Mo	0.045	0.106	0.119	0.731	Μo	0.015
	8 0	0.227	0.143	0.631	Mo		0.370	0 183	0.447	Mo		0.122	0.165	60.40	Mo	
	81	0.353	0.364	0.284	Mmicro	0.048	0.412	0.359	0.229	Мтасго	0.101	0.279	0.371	0.350	Mmicro	0.033
	83	0.348	0.371	0.281	Mmicro	0.026	0.406	0.386	0.228	Мтасго	0.058	0.276	0.379	0.345	Mmicro	0.019
-	88	0.356	0.371	0.274	Mmicro	0.034	0.413	0.365	0.222	Мтасго	0.073	0.284	0.378	0.338	Mmicro	0.023
	84	0.350	0.379	0.271	Mmicro		0.409	0.372	0.219	Мпасго		0.273	0.386	0.337	Mmicro	
**s	81	0 208	0.215	0.567	Mo	0.032	0.321	0.242	0.437	Мо	0.078	0.100	0.244	0.656	Mo	0.022
	88	0.206	0.243	0.551	Мо	0.018	0.315	0.256	0.428	Мо	0.039	0.103	0.260	0.637	Mo	0,013
	88	0.219	0.242	0.539	Mo	0.022	0.326	0.256	0.419	Мо	0.049	0.115	0.260	0.625	Мо	0.016
	*	0.207	0.252	0.541	Mo		0.318	0 264	0.418	Mo		0.102	0.269	0.630	Mo	
	81	0.430	0.342	0.229	Mmacro	0.079	0.486	0.339	0,175	Mmacro	0,163	0.344	0.355	0.305	Mmicro	0.057
	88	0.422	0.351	0.227	Mmacro	0.046	0.478	0.348	0.175	Мтасго	0.097	0.339	0.361	0.301	Mmicro	0,032
:	53	0.431	0.350	0.219	Мпасго	0.057	0.485	0.347	0.168	Mmacro	0.120	0.347	0.353	0.293	Mmicro	0.040
 10 11	8	0.427	0.359	0.215	Мтасго		0.482	0.354	0.164	Мтасго		0.341	0.301	0.291	Мшісго	
	8	0.307	0.156	0.537	Mo	0.064	0.421	0.190	0.391	Мтасго	0,115	0.171	0.183	0.646	Mo	0.038
	88	008.0	0.181	0.519	Μ°	0.031	0.411	0.209	0.380	Мтасго	0.067	0.171	0.205	0.624	Mo	0.022
=	5	0.816	0.180	0.504	Mo	0.038	0.422	0.208	0.370	Мшасго	0.083	0.185	0.205	0.610	Mo	0.027
	8	0.304	0.190	0.506	Mo		0.416	0.216	0,368	Мпасго		0 171	0.214	0,625	Mo	

Table 8, the two inspective "prediction" results for variou's large reservoirs are listed in the last two row.

It is not difficult to find out that SEM is less successful. According to its predictions, examination probabilites can reach or approach 0.5 only for 12 induced reservoirs, with a success rate of only about 40%, and at the same time seismoinductive intensity can not be predicted.

On the contrary, FCEM has a success rate of "prediction" of up to 70% for $M_s \ge 5$, 80% for $M_s < 5$ and 85% for M_s (assume that the fault

activity is f₂). Therefore conclusion may be drawn that with the existing data-based FCEM, it is possible to estimate with 70.80% of certainty the seisminductive risk and the possible maxmum intensity of large new reservoirs.

Of couse, FCEM still has some aspects to be improved which are not to be discussed here.

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预测水库诱发地震的两个数学模式

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摘 要

近几十年来,特别是近二十年来,随着人类工程活动的规模和领域的扩大,出现了伴生的新问题——诱发地震。水库蓄水、小规模的地面或地下采矿、处理废液、地热发电和石油开采及城市大量抽取地下水以及地下核爆破等都造成局部地震活动增强。由于诱发地震是伴随大型工程而发生的,且多发生于大型工程附近,所以即使5级左右的地震也应予以考虑。

国内外学者对水库地震的预测提出过许多方法。本文介绍了预测水库地震的统计检验预测模式和两级模糊综合评判模式, 並用实 际水 库震 例进 行了检验。